# An Alternative Method for the Estimation of Critical Temperatures of Mixtures

C. A. Castillo S.

Chemistry Department Universidad del Valle Apartado aéreo 25360 Cali, Colombia

A knowledge of the critical temperature of mixtures is important, and because of the difficulty of measuring the critical properties of mixtures experimentally, it is desirable to have reliable methods for correlating and predicting these properties. A survey of the literature indicates that a variety of correlations have been advanced for predicting the critical temperature of mixtures. For example Spencer et al. (1973) reviewed and evaluated a number of proposed methods for estimating the critical temperatures of mixtures. In this note a new alternative method, based on the heat capacity fraction, is proposed to correlate experimentally determined critical temperatures.

If the composition of a mixture is expressed as

$$\delta i = \frac{Y_i C v_i}{\sum Y_i C v_i} \tag{1}$$

the mixture's critical temperature can be estimated by

$$T_{cm} = \sum \delta i \ T_{ci} \tag{2}$$

where  $y_i$  is the mole fraction of i,  $C_{v_i}$  the molal heat capacity of i,  $T_{c_i}$  the critical temperature of i, and  $T_{cm}$  the mixture critical temperature. Here our attention is restricted to normal fluids; that is, to molecules that have zero (or small) dipole moments, no tendency to associate by hydrogen bonding or similar chemical forces, and that have sufficiently large mass to permit neglect of quantum corrections.

In figure 1, the critical temperature of three binary systems—methane-propane (Reamer et al., 1950); methane-n-butane (Sage et al., 1940); and methane-n-pentane (Sage et al, 1942)—are shown plotted as a function of mole fraction (open symbols) and heat capacity fraction (closed symbols). It is clear that the use of heat capacity fractions provides essentially a linear relationship between  $\delta i$  and  $T_{cm}$ , as predicted by Eq. 2. Table 1 lists literature data employed for the calculations.

The behavior of the binary hydrocarbon mixtures that have

been investigated raises the possibility of using this nearly linear property to estimate the critical temperature of ternary systems of hydrocarbons. To establish these values only the critical temperature and the molal heat capacity data for each component is required. The approach to the estimation of such temperatures is as follows.

Since the critical temperature is not known, values must be assumed and the answer can be reached by a series of successive approximations. As a starting assumption the molal average pseudocritical temperature of the mixture  $(T_{cp} = \sum_i y_i T_{c_i})$  can be taken as equal to the temperature sought. This allows us to calculate the heat capacity fraction, Eq. 1, and the desired temperature, Eq. 2. The procedure is repeated until the new calculated value of  $T_{cm}$  checks with the last calculated value. The search procedure is straightforward and does not in general require a large number of iterations to find the critical temperature. To illustrate this method of calculation the following example is presented.

## Example

Determine the critical temperature of a ternary mixture having the following composition

	Mol Frac.
Methane	0.480
Propane	0.265
n-Pentane	0.255
	1.000

Step A. From the data in Table 1 we calculate the molal average pseudocritical temperature for this mixture. The starting assumption is:

$$T_{op} = 0.48(190.6) + 0.265(396.8) + 0.255(469.6)$$
  
= 309 K.

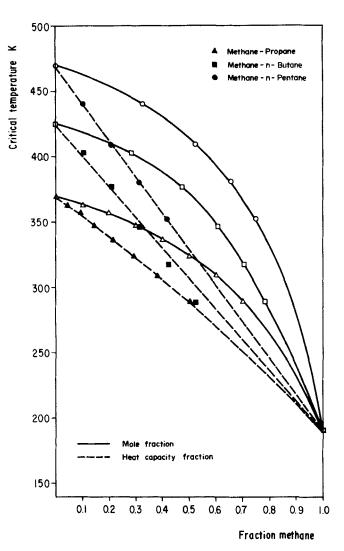


Figure 1. Critical temperatures of three binary methane systems as a function of mole fraction and heat capacity fraction.

△□○ Mole fraction

A ■ Heat capacity fraction.

Table 1. Literature Data for Calculations Plotted in Figure 1 (Reid et al., 1977)

Crit. Temp. Compound K		Constants in Ideal Gas Heat Capacity Eq.* cal/mol·K		
	•	A	$B \times 10^2$	$C \times 10^5$
Methane	190.6	2.611	1.245	0.286
Propane	369.8	-2.966	7.315	-3.789
n-Butane	425.2	0.279	7.913	-2.647
n-Pentane	469.6	-2.853	11.64	-6.163

<sup>\*</sup> $A + BT + CT^2 - R$ R, universal gas constant = 1.987 cal/mol · K

Using Eq. 1:

		Heat
	$C_v$ at 309 K	Capacity
	cal/mol · K	Frac.
Methane	6.374	0.2239
Propane	16.031	0.2937
n-Pentane	27.248	0.4824
		1.000

With Eq. 2:

$$T_{cm} = 0.2239(190.6) + 0.2937(36.8) + 0.4824(496.6)$$
  
= 377.8 K.

Step B. At T = 377.8 K, using Eq. 1:

		Heat
	C <sub>v</sub> at 377.8 K	Capacity
	cal/mol·K	Frac.
Methane	7,723	0.2171
Propane	19,262	0.2985
n-Pentane	32,326	0.4843
		1.000

With Eq. 2:

$$T_{cm} = 0.2171(190.6) + 0.2985(369.8) + 0.4843(469.6)$$
  
= 379.2 K.

Step C. At 379.2 K, with Eq. 1:

	C <sub>v</sub> at 379.2 K	Heat Capacity
	_cal/mol K_	Frac.
Methane	7,743	0.2174
Propane	19,324	0.2990
n-Pentane	32,424	0.4836
		1.000

With Eq. 2:

$$T_{cm} = 379.1 \text{ K } (222.4^{\circ}\text{F}).$$

For this particular ternary composition, Grieves and Thodos (1962) report a critical temperature of  $220^{\circ}F$  (104°C)  $\times$  (377.8K).

There is also an alternative procedure to calculate  $T_{cm}$ . The heat capacity of each component can be estimated from the principles of statistical mechanics, in which the total internal energy is made equal to the sum of the energies due to the translational and rotational motions of the molecule and to the vibrational motion of the atoms making up the molecules.

The theory of equipartition of energy provides a means of estimating the molal heat capacity of a gas. According to this theory, each translational and rotational degree of freedom contributes R/2 to Cv, while the maximum vibrational contribution is R, where R = gas constant. Since, there is a total of 3N (N = number of atoms in the molecule) degrees of freedom, the molal heat capacity for a nonlinear molecule (three rotational degrees

of freedom) becomes:

$$Cv = 3R/2 + 3R/2 + (3N - 6)R = 3(N - 1)R$$

The previously-mentioned example then can be solved by this method. The molal heat capacities and the values of  $\delta i$ , calculated using Eq. 1 are:

	Cv	$\delta i$
Methane	12 <i>R</i>	0.222
Propane	30 <i>R</i>	0.306
n-Pentane	48 <i>R</i>	0.472
		1.000

Using Eq. 2, we obtain:

$$T_{cm} = (0.222)(190.6) + (0.306)(369.8) + (0.472)(469.6)$$
  
= 377.1 K.

This agreed reasonably well with the iterative method described earlier.

# **Acknowledgment**

The author wishes to thank R. Paredes for review of the manuscript and for helpful suggestions.

#### Notation

 $C_{v_i}$  = molal heat capacity at constant volume of component i

R = gas constant

T - temperature

 $T_{c_i}$  = critical temperature of component i

 $T_{cm}$  = critical temperature of a mixture  $T_{cp}$  = pseudocritical temperature

 $y_i$  = mole fraction of component i

 $\delta i$  = heat capacity fraction

## Subscripts

c = critical

i = pure component i

m = mixture

#### Literature cited

Grieves, R. B., and G. Thodos, "The Critical Temperatures of Ternary Hydrocarbon Systems," Ind. Eng. Chem. Fundam., 1, 45 (1962).

Reamer, H. H., B. H. Sage, and W. N. Lacey, "Phase Equilibria in Hydrocarbon Systems: Volumetric and Phase Behavior of the Methane-Propane System," Ind. Eng. Chem., 42, 534 (1950).

Reid, R. C., J. M. Prausnitz, and T. K. Sherwood, The Property of Gases and Liquids, 3rd ed., McGraw-Hill, New York, Appendix A, "Property Data Bank," (1977).

Sage, B. H., B. L. Hicks, and W. N. Lacey, "Phase Equilibria in Hydrocarbon Systems: The Methane-n-Butane System in the Two-Phase

Region," Ind. Eng. Chem., 32, 1085 (1940).
Sage, B. H., H. H. Reamer, R. H. Olds, and W. N. Lacey, "Phase Equilibria in Hydrocarbon Systems: Volumetric and Phase Behavior of the

Methane-n-Pentane System," Ind. Eng. Chem., 34, 1108 (1942). Spencer, C. F., T. E. Daubert, and R. P. Danner, "A Critical Review of Correlations for the Critical Properties of Defined Mixtures," AIChE J., 19, 522 (1973).

Manuscript received June 23, 1986, and revision received Sept. 17, 1986.